

Safety performance based departures from geometric design requirements

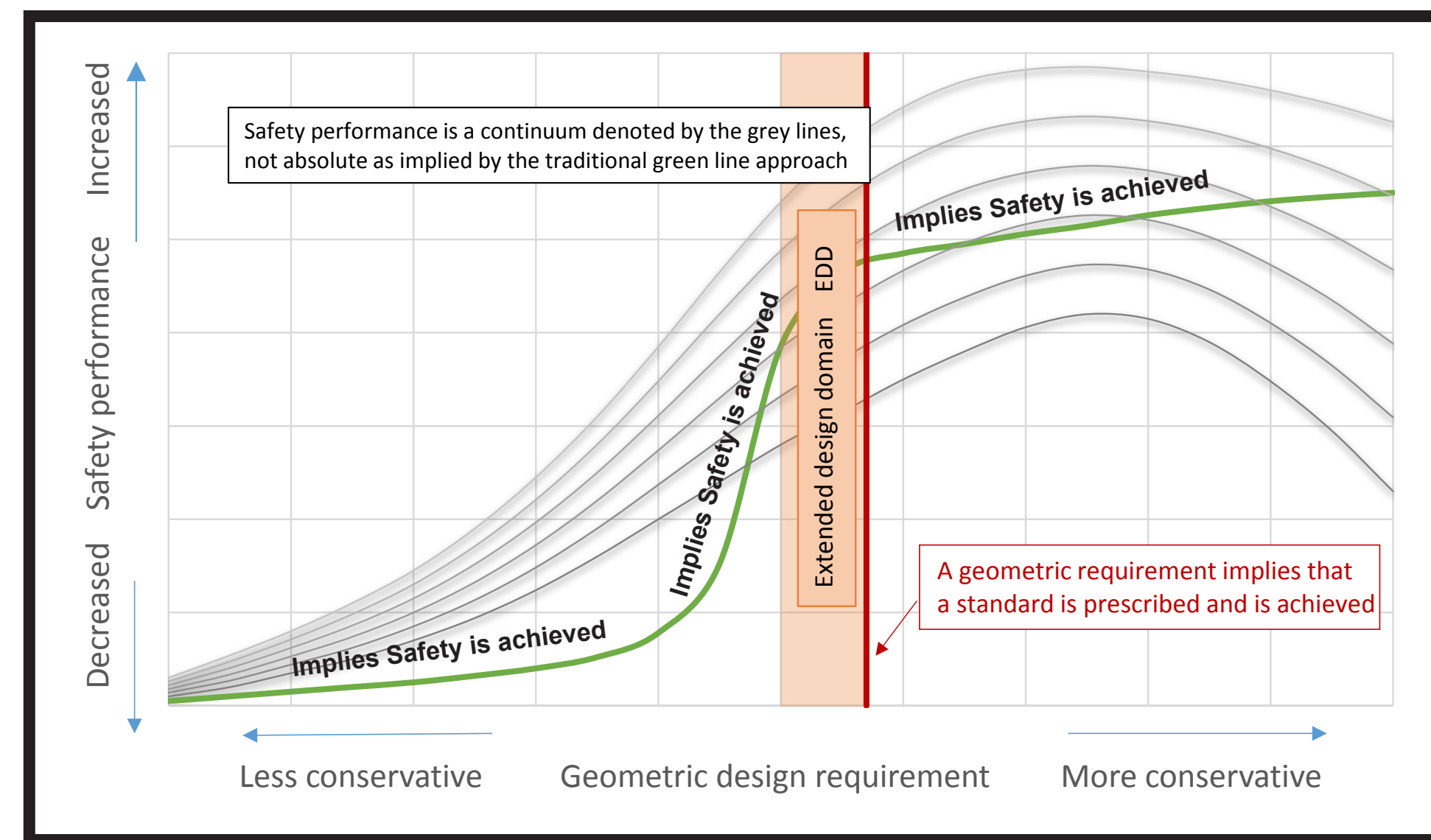
IPENZ Transportation Group Conference 2016 - Paper 51



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This is a worked example showing the different results for stopping sight distance and crest vertical curvature when using a probabilistic approach versus the traditional deterministic (manuals and guidelines) approach.

TRADITIONAL DETERMINISTIC APPROACH



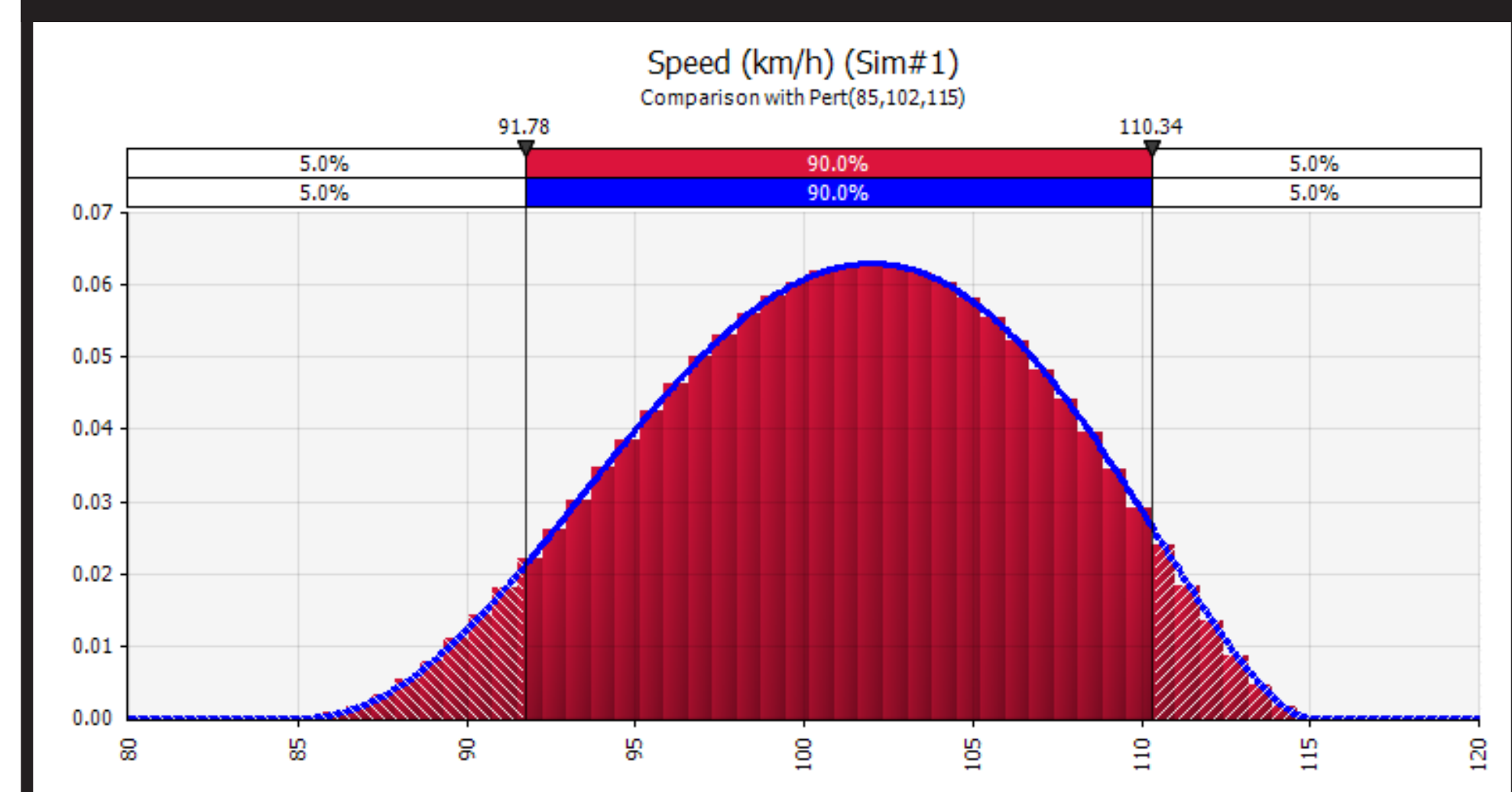
Manuals and Guidelines

Example of deterministic design parameters for a motorway

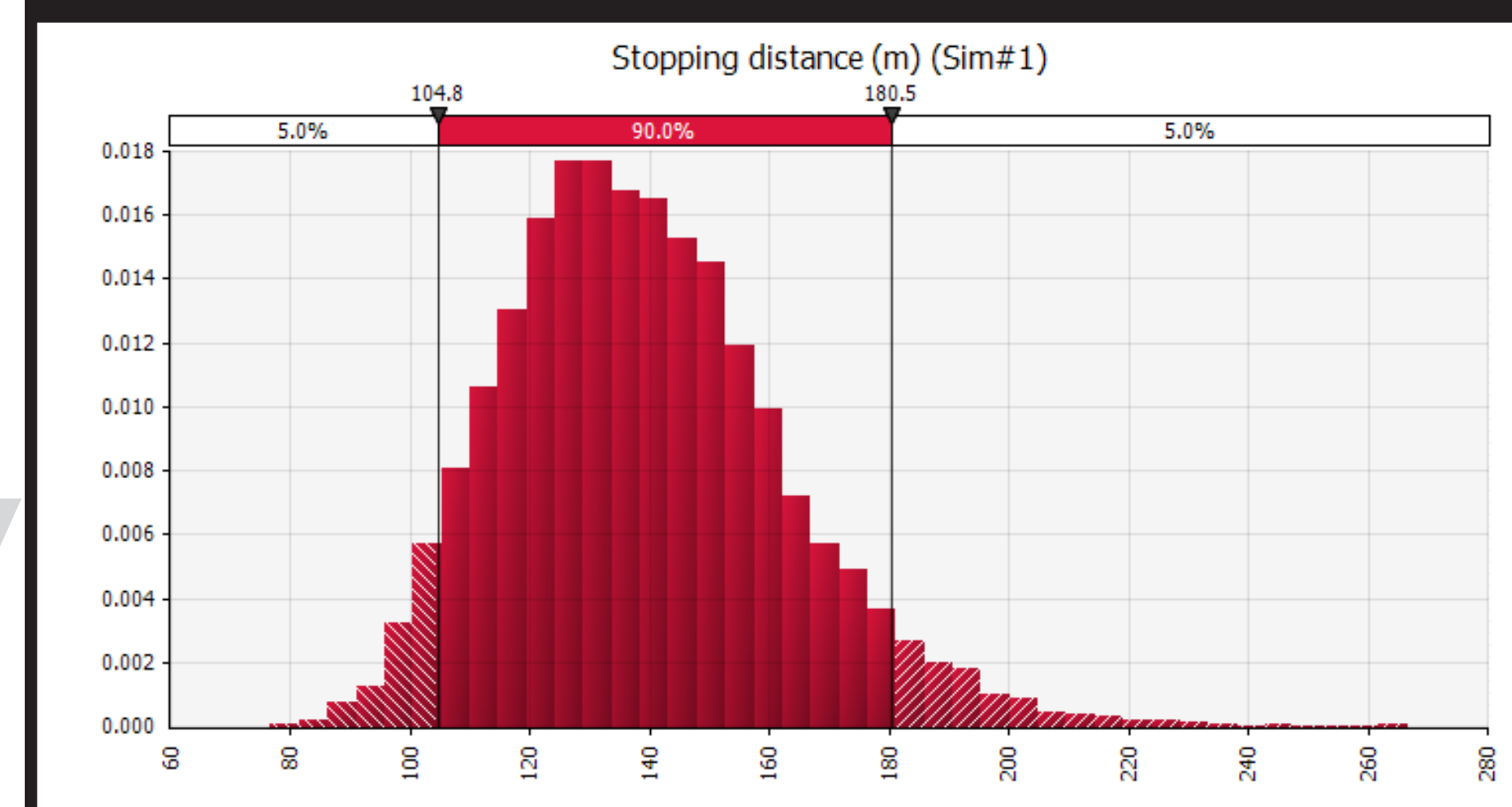
Design Speed	Perception & Reaction Time	Deceleration Coefficient	Stopping Sight Distance	Driver Eye Height	Object Height	Crest Curvature
V	RT	d	S	h ₁	h ₂	K
km/h	s		m	m	m	m/1%
110	2.5	0.26	260	1.1	0.2	151
110	2.5	0.36	209	1.1	0.2	97
110	2.5	0.46	180	1.1	0.2	72

PROBABILISTIC APPROACH

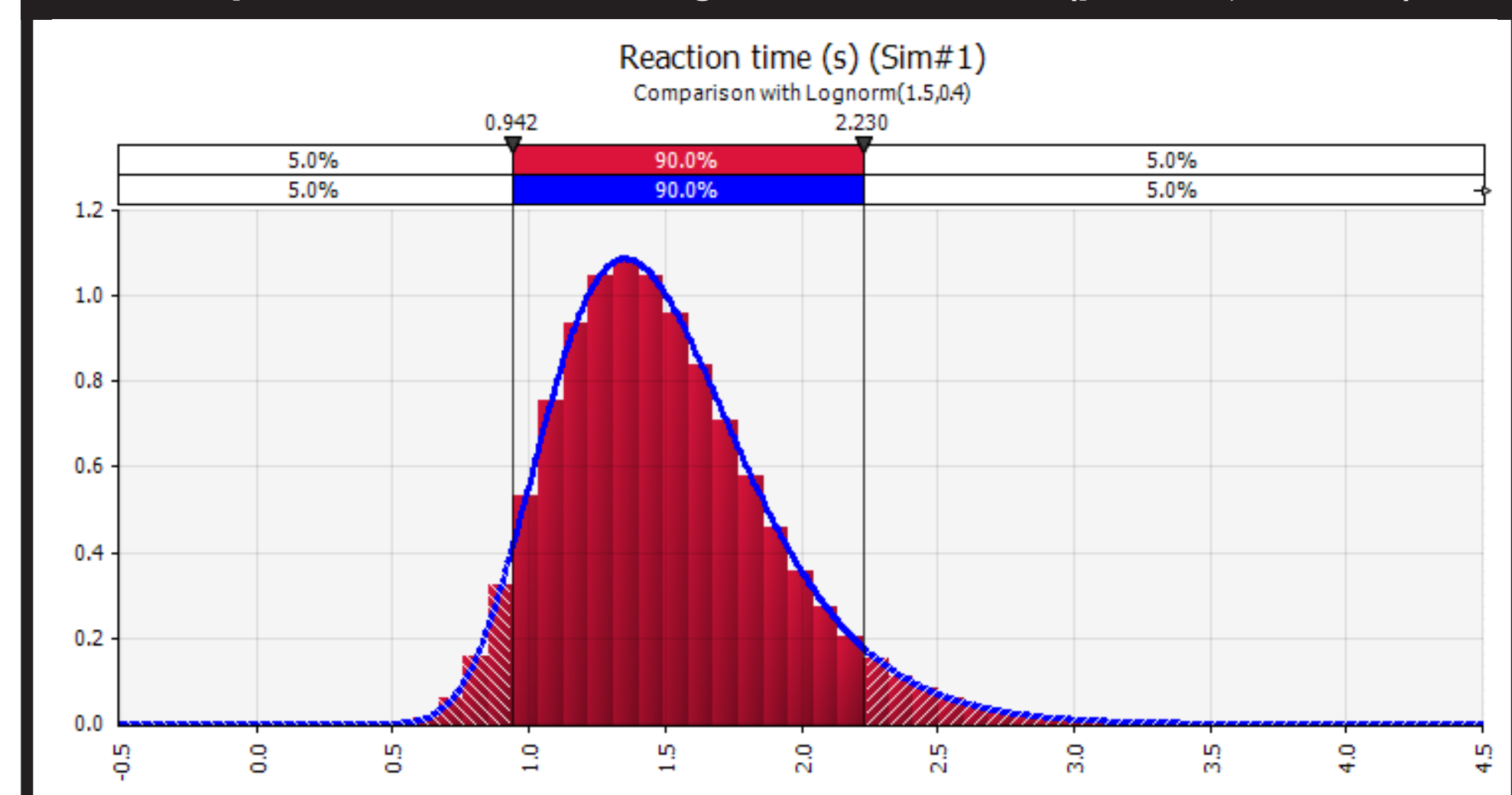
Operating speed Pert distribution (Vmin = 85 km/h, μ = 102 km/h, Vmax = 115 km/h)



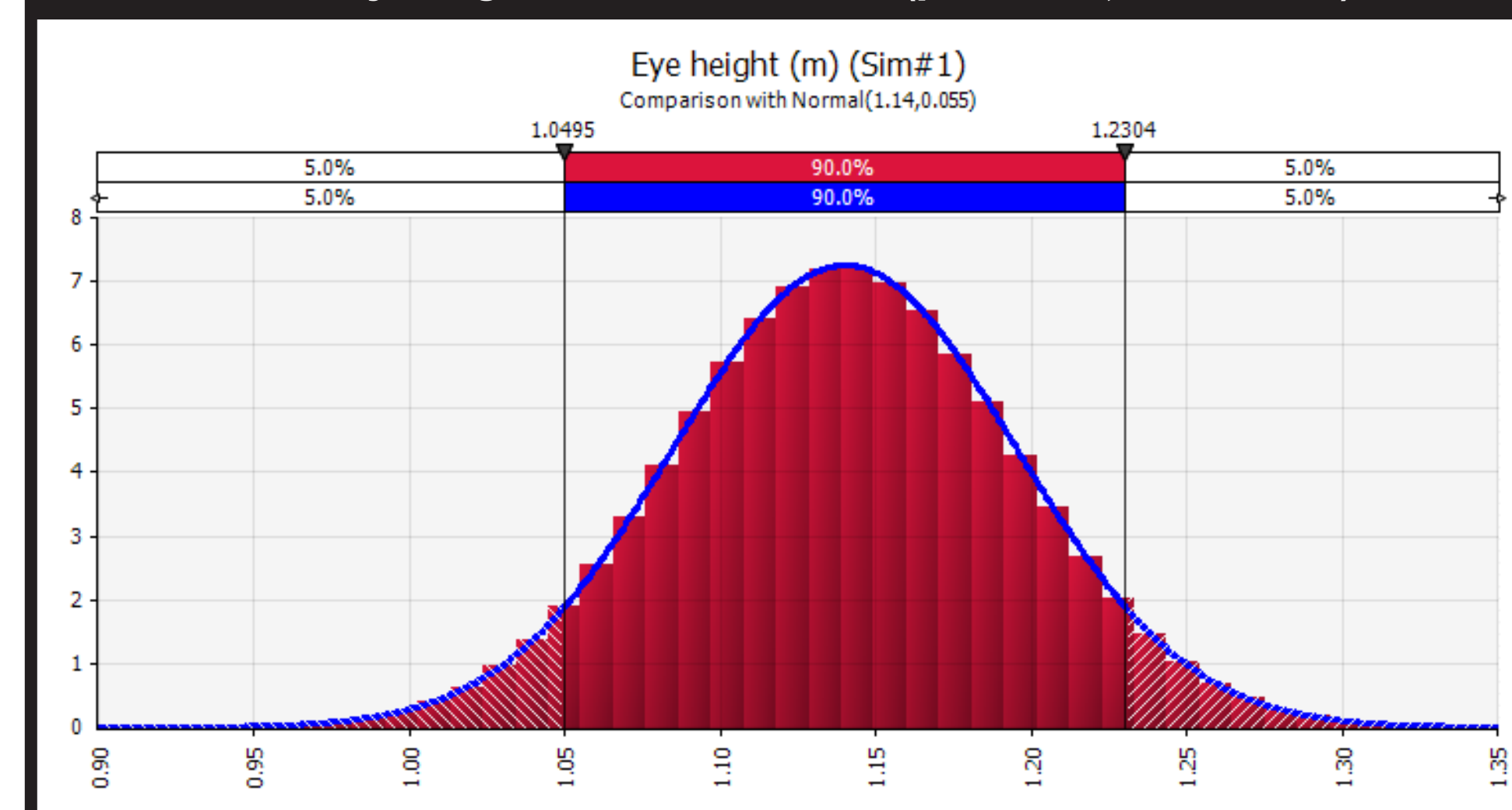
Stopping distance distribution



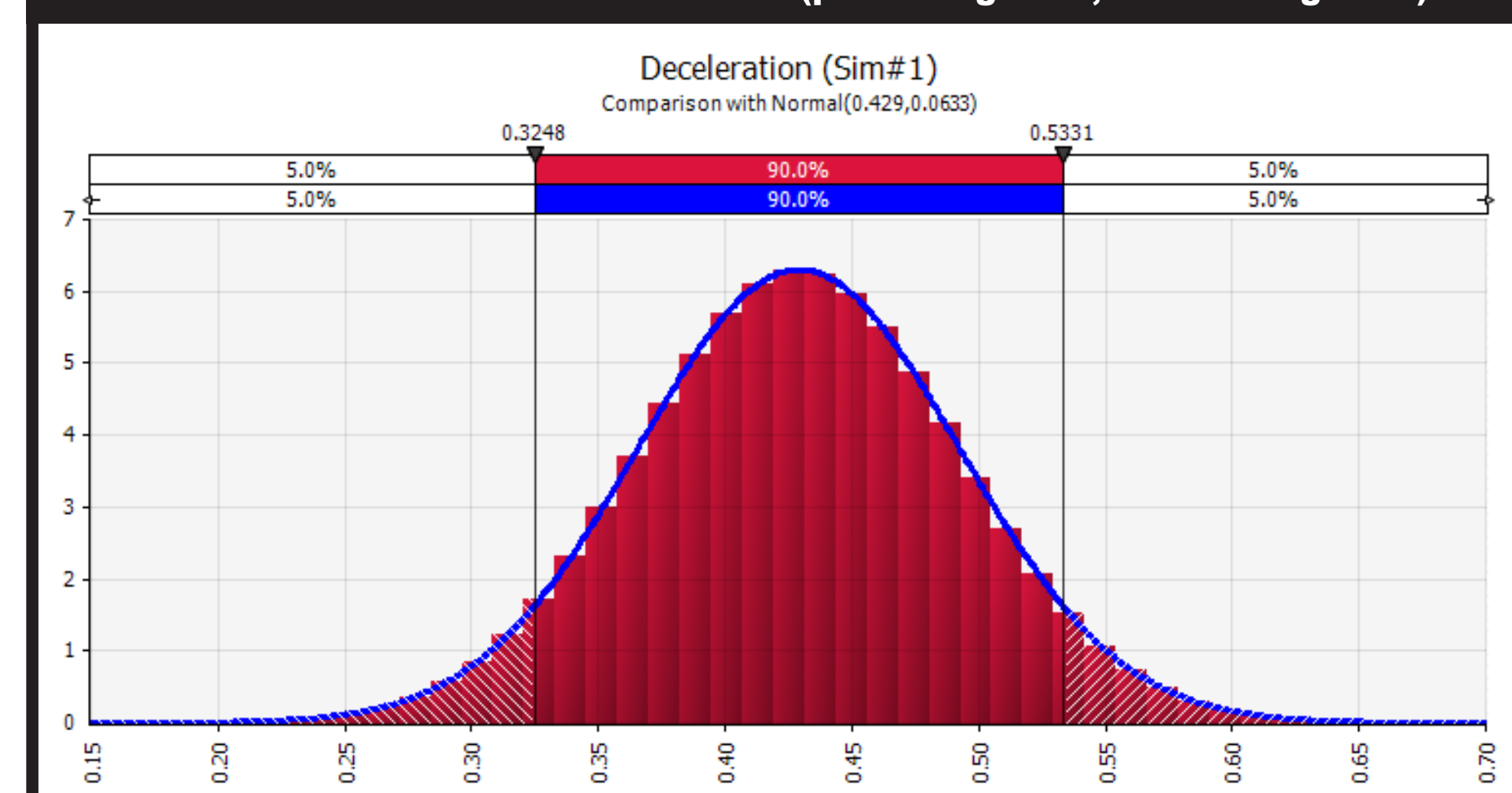
Perception and reaction time lognormal distribution (μ = 1.5 s, σ = 0.4 s)



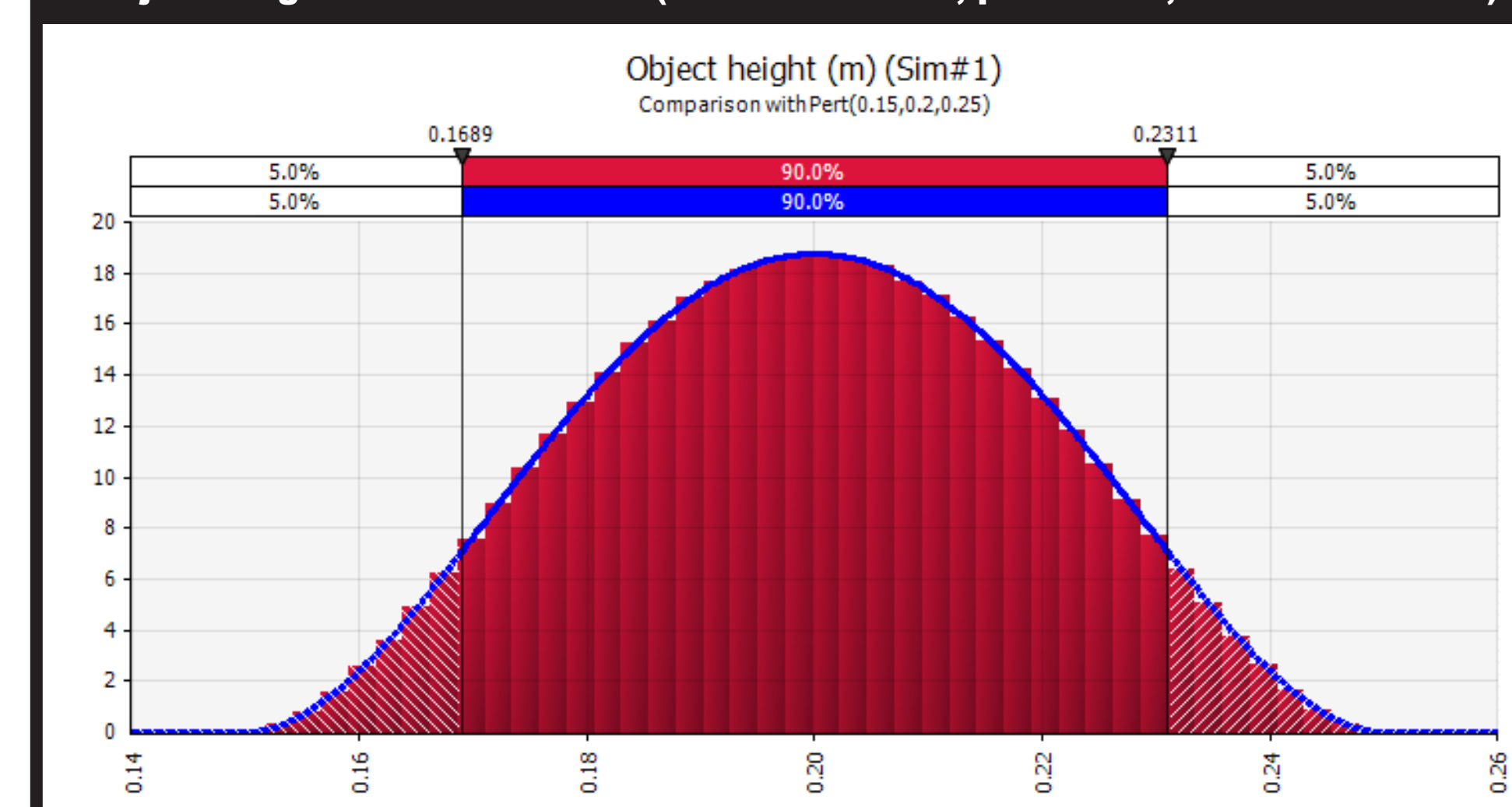
Driver eye height normal distribution (μ = 1.14 m, σ = 0.055 m)



Deceleration rate normal distribution (μ = 0.429g m/s², σ = 0.0633g m/s²)



Object height Pert distribution (h2 min = 0.15 m, μ = 0.20 m, h2 max = 0.25 m)



Monte Carlo Simulation

Monte Carlo Simulation

Stopping sight distance formula

$$SSD = \frac{R_1 V}{3.6} + \frac{V^2}{254(d + 0.01a)}$$

SSD = stopping sight distance (m)
 RT = driver perception and reaction time (s)
 V = vehicle speed (km/h)
 d = deceleration coefficient
 a = longitudinal gradient (%)

Crest vertical curvature formula

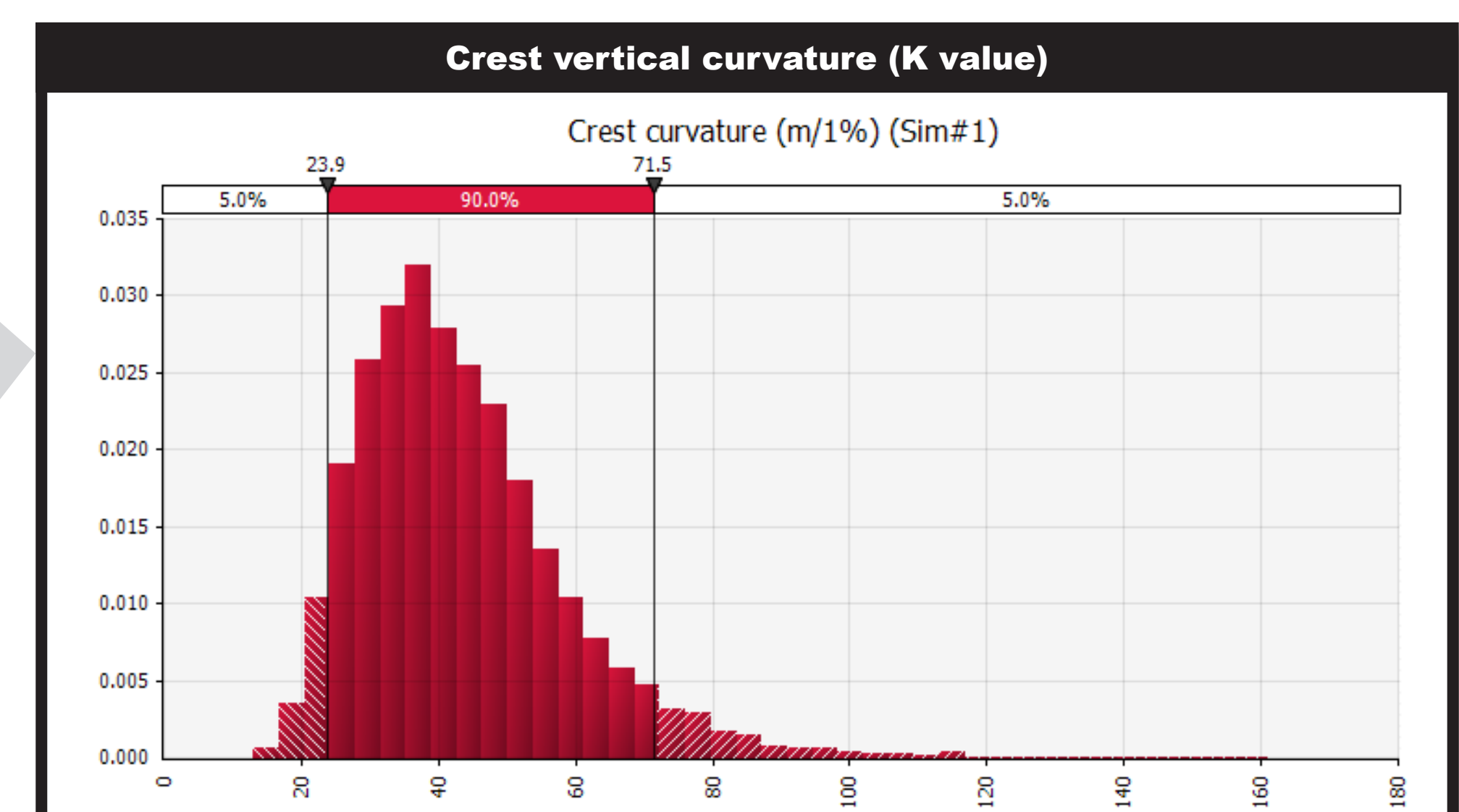
$$K = \frac{S^2}{200(\sqrt{h_1} + \sqrt{h_2})^2}$$

K = vertical curvature (m/1%)
 S = distance (m)
 h₁ = driver eye height (m)
 h₂ = observed object height (m)

- These distributions can all be modified by design, for example:
- reduce speed with side friction
 - decrease reaction time by increasing driver awareness with street lighting
 - increase deceleration rates with high friction surfaces

Compare the Results

	Operating speed distribution	Perception & reaction time distribution	Deceleration coefficient distribution	Resultant SSD distribution	Driver eye height distribution	Object height distribution	Resultant crest curvature distribution
	V	RT	d	S	h ₁	h ₂	K
	km/h	s		m	m	m	m/1%
0.1%	87	0.6	0.23	85	0.97	0.15	16
0.5%	88	0.7	0.27	92	1.00	0.16	18
1.0%	89	0.8	0.28	95	1.01	0.16	19
5.0%	92	0.9	0.32	105	1.05	0.17	24
10.0%	94	1.0	0.35	111	1.07	0.17	27
50.0%	101	1.4	0.43	137	1.14	0.20	41
90.0%	109	2.0	0.51	169	1.21	0.23	63
95.0%	110	2.2	0.53	181	1.23	0.23	71
99.0%	113	2.7	0.58	204	1.27	0.24	91
99.5%	113	2.8	0.59	214	1.28	0.24	99
99.9%	114	3.3	0.62	232	1.31	0.25	116



The next steps

- The probability of stopping in time can now be correlated with a known crash history on a representative road, so that a particular probability will correlate with an expected number of fatal crashes per 100,000 vehicle kilometres.
- Future designers will target a safety outcome and therefore a specified probability of stopping, instead of relying on the assumption that using the default design speed, reaction time, and deceleration rate will always achieve that outcome.